

CHAPTER 1 MAGNETIC AND MAGNETICALLY COUPLED CIRCUITS

Short Problems

SP 1.2-1

$$Z = \frac{\tilde{V}}{\tilde{I}} = 1 \angle 180^\circ = -1$$

$$S = \tilde{V}\tilde{I} = -1 \text{ W}$$

Negative indicates generator operation.

SP 1.2-2

$$V(t) = \sqrt{2} \cos(377t)$$

$$I(t) = \sqrt{2} \cos(377t + \pi)$$

$$P(t) = V(t)I(t) = -2 \cos^2(377t) = -1 - \cos(754t) = -1 + \cos(754t + \pi)$$

SP1.2-3

$$A + B = \sqrt{2}(1 + j) = \sqrt{2}\sqrt{2}(1 \angle 45^\circ) = 2 \angle 45^\circ$$

$$AB = \sqrt{2}\sqrt{2}j = 2j = 2 \angle 90^\circ$$

SP 1.2-4 For simplicity, and without lack of generality, neglect resistance and assume the voltage is along the real axis. In this case the relationship between voltage and current is given by:

$$V \angle 0 = j(X_L - X_C)\tilde{I} + \tilde{E}$$

One can observe that the magnitude and phase of \tilde{E} controls the magnitude and direction of \tilde{I} . For example, if $\tilde{E} = 2 \angle 0^\circ$ and $X_L > X_C$, \tilde{I} will lead \tilde{V} . In contrast, if $\tilde{E} = 0.5 \angle 0^\circ$ and $X_L > X_C$, \tilde{I} will lag \tilde{V} .

SP1.3-1. $Ni = \mathcal{R}_{ab}(\Phi_1 + \Phi_2) + \mathcal{R}_{bcda}\Phi_1$

$$\Phi_1 = \frac{1}{\mathcal{R}_{bcda}} [Ni - \mathcal{R}_{ab}(\Phi_1 + \Phi_2)]$$

$$\Phi_1 = \frac{1}{358,099} \left[-(109,419)(2.547 \times 10^{-3}) \right] = 2.014 \times 10^{-3} \text{ Wb}$$

SP1.3-2. $\tilde{\Phi}_1 + \tilde{\Phi}_2 = \frac{N\tilde{I}}{\mathcal{R}_{ab} + \mathcal{R}_{eq}}$

$$= \frac{(100) 10 \angle -30^\circ}{109,419 + 283,148} = 2.547 \times 10^{-3} \angle -30^\circ \text{ Wb, rms}$$

SP1.3-3. With windings as shown in Fig. 1B-1 and with the center leg removed, the total mmf is

$$\begin{aligned}\text{mmf}_t &= \text{mmf}_1 + \text{mmf}_2 = N_1 I_1 + N_2 I_2 \\ &= (150)(9) + (90)(-15) = 0\end{aligned}$$

SP1.3-4

$$\begin{aligned}\tilde{\phi}_2 &= \sqrt{1.065^2 + 0.427^2} \times 10^{-3} < \tan^{-1}\left(\frac{0.427}{1.065}\right) \\ \tilde{\phi}_2 &= \sqrt{2} \cdot 1.147 \times 10^{-3} \cos(\omega t + 21.8^\circ)\end{aligned}$$

SP1.4-1. From Fig. 1.3-1, $H_i = 200$ A/m for $B_i = 1$ Wb/m². Also,

$$H_g = \frac{B_g}{\mu_0} = \frac{1}{4\pi \times 10^{-7}} = 7.958 \times 10^5 \text{ A/m.}$$

From (1.3-3),

$$\begin{aligned}H_i l_i + H_g l_g &= NI \\ (200)(1) + (7.958 \times 10^5)(0.001) &= (500)I\end{aligned}$$

Thus, $I = 1.99$ A

SP1.5-1. $\mathcal{R}_m = 2\mathcal{R}_y = (2)(37,600) \text{ H}^{-1}$

$$L_{11} = \frac{N_1^2}{\mathcal{R}_m} = \frac{(150)^2}{(2)(37,600)} = 299.2 \text{ mH}$$

$$L_{22} = \frac{N_2^2}{\mathcal{R}_m} = \frac{(90)^2}{(2)(37,600)} = 107.7 \text{ mH}$$

$$L_{12} = \frac{N_1 N_2}{\mathcal{R}_m} = \frac{(150)(90)}{(2)(37,600)} = 179.5 \text{ mH}$$

SP1.5-2. During steady-state conditions, the time rate-of-change of i_1 is zero; therefore, a voltage is not induced in the 2-winding. Hence, for the 2-winding open or short

circuited $I_1 = \frac{V}{r_1} = \frac{12}{6} = 2$ A and $I_2 = 0$.

SP1.5-3. $Z = r_1 + j\omega_e(L_{11} + L_{m1}) = 6 + j(100)(13.5 + 263.9) \times 10^{-3}$

$$= 6 + j27.74 = 28.38 \angle 77.8^\circ$$

$$\tilde{I}_1 = \frac{\tilde{V}_1}{Z} = \frac{10 \angle 0^\circ}{28.38 \angle 77.8^\circ} = 0.352 \angle -77.8^\circ \text{ A}$$

SP1.6-1. The peak-to-peak value of λ as the system approaches steady-state operation is $(0.95)(\sqrt{2})(0.29) = 0.389$ V·s. Now, $\lambda = L_{m1}(i_1 + i_2')$ or $i_1 + i_2' = \frac{\lambda}{L_{m1}}$. The ampli-

tude of $i_1 + i_2' = \frac{0.389}{(2)(263.9 \times 10^{-3})}$. Hence,

$$|\tilde{I}_1 + \tilde{I}_2'| = \frac{0.389}{(\sqrt{2})(2)(263.9 \times 10^{-3})} \cong 0.5 \text{ A}$$

SP1.6-2. $Z = (r_1 + r_2') + j\omega_e(L_{11} + L_{12}')$

$$\phi = \tan^{-1} \frac{\omega_e(L_{11} + L_{12}')}{r_1 + r_2'} = \tan^{-1} \frac{(377)(13.5 + 13.5) \times 10^{-3}}{6 + 5} = 42.8^\circ$$

SP1.6-3. $Z = (r_1 + r_2' + R_L') + j[\omega_e(L_{11} + L_{12}') + X_L']$
 $= (6 + 5 + 21) + j[(1000)(13.5 + 13.5) \times 10^{-3} + 5] = 32 + j32 \Omega$

$$\tilde{I}_2' \cong -\tilde{I}_1 = -\frac{\tilde{V}_1}{Z} \cong \frac{-110 \angle 0^\circ}{32 + j32} \cong -2.4 \angle -45^\circ$$

SP1.7-1.
$$\begin{aligned} \frac{d[L_m(x)i]}{dt} &= \frac{\partial[L_m(x)i]}{\partial i} \frac{di}{dt} + \frac{\partial[L_m(x)i]}{\partial x} \frac{dx}{dt} \\ &= L_m(x) \frac{di}{dt} + i \frac{\partial L_m(x)}{\partial x} \frac{dx}{dt} \\ &= \frac{k}{x} \frac{di}{dt} + i \left(-\frac{k}{x^2}\right) \frac{dx}{dt} \end{aligned}$$

Now, $x = t$ and $i = t$; thus,

$$\frac{d[L_m(x)i]}{dt} = \frac{k}{t} \frac{dt}{dt} - t \frac{k}{t^2} \frac{dt}{dt} = \frac{k}{t} - \frac{k}{t} = 0$$

SP1.7-2. For $\theta_r(0)$, \mathcal{R} is minimum thus $L(\theta_r)$ is maximum. Hence,

$$L_m(0) = L_A + L_B$$

$$L_m\left(\frac{\pi}{2}\right) = L_A - L_B; \text{ thus,}$$

$$L(\theta_r) = L_1 + L_A + L_B \cos 2\theta_r$$

SP1.7-3. The self-inductances, L_{11} and L_{22} , are independent of current if saturation is neglected; therefore, they are unchanged. The mutual inductance is positive if the mmfs aid and negative when they oppose. Here, the mmfs oppose when $\theta_r = 0$ and aid when $\theta_r = \pi$. Thus,

$$L_{12} = -L_{sr} \cos \theta_r$$

$$\text{SP1.7-4. } L_{12} = L_{sr} \cos \theta_r$$

$$v_2 = \frac{d[L_{12} i_1]}{dt} = \frac{\partial[L_{12} i_1]}{\partial i_1} \frac{di_1}{dt} + \frac{\partial[L_{12} i_1]}{\partial \theta_r} \frac{d\theta_r}{dt}$$

However, $\frac{di_1}{dt} = 0$ since i_1 is constant; thus,

$$v_2 = \frac{\partial[(0.1 \cos \theta_r)(1)]}{\partial \theta_r} (100) = -(0.1)(100) \sin \theta_r = -10 \sin 100t \text{ V}$$

Long Problems

$$1. \quad \mathcal{R}_g = \frac{l_g}{\mu_g A_g} = \frac{0.004}{(4\pi \times 10^{-7})(0.04)^2} = 1,989,440 \text{ H}^{-1}$$

$$\mathcal{R}_i = \frac{l_i}{\mu_i A_i} = \frac{(200)(0.004)}{(1500)(4\pi \times 10^{-7})(0.04)^2} = \frac{200}{1500} \mathcal{R}_g = 265,258 \text{ H}^{-1}$$

$$\Phi = \frac{Ni}{\mathcal{R}_g + \mathcal{R}_i} = \frac{(100)(2)}{1,989,440 + 265,258} = 8.87 \times 10^{-5} \text{ Wb}$$

2. The parallel branches now have equal reluctance. Hence, from Example 1A

$$\mathcal{R}_{eq} = \frac{1}{2} (\mathcal{R}_{bef} + \mathcal{R}_{fg} + \mathcal{R}_{gha}) = \frac{1}{2} (1,352,816) = 676,408 \text{ H}^{-1}$$

$$\Phi_1 + \Phi_2 = \frac{Ni}{\mathcal{R}_{ab} + \mathcal{R}_{eq}} = \frac{(100)(10)}{109,419 + 676,408} = 1.2725 \times 10^{-3} \text{ Wb}$$

3. The reluctance of the iron is

$$\mathcal{R}_m = \frac{l}{\mu_i A} = \frac{(4)(0.25)}{(4000)(4\pi \times 10^{-7})(0.05)^2} = 79,577 \text{ H}^{-1}$$

$$L_{12} = \frac{N_1 N_2}{\mathcal{R}_m} = \frac{(50)(100)}{79,577} = 0.0628 \text{ H}$$

$$L_{m1} = \frac{N_1^2}{\mathcal{R}_m} = \frac{50^2}{79,577} = 0.0314 \text{ H}$$

$$L_{m2} = \frac{N_2^2}{\mathcal{R}_m} = \frac{100^2}{79,577} = 0.1257 \text{ H}$$

$$4. \quad \mathcal{R}_m = \frac{1}{\mu A} = \frac{(2\pi)(1)}{(4\pi \times 10^{-7})\left(\frac{1}{4\pi} \times 10^4\right)\pi(0.05)^2} = 8 \times 10^5 \text{ H}^{-1}$$

$$L_{12} = -\frac{N_1 N_2}{\mathcal{R}_m} = -\frac{(100)(200)}{8 \times 10^5} = -25 \text{ mH}$$

5. The flux through N_2 due to current in N_1 may be written

$$\Phi_{21} = \frac{\mathcal{R}_x}{\mathcal{R}_x + \mathcal{R}_y} \frac{N_1 i_1}{\mathcal{R}_m}$$

where $\mathcal{R}_m = 10\mathcal{R}_y + \frac{\mathcal{R}_x \mathcal{R}_y}{\mathcal{R}_x + \mathcal{R}_y}$; thus,

$$\Phi_{21} = \frac{N_1 i_1}{11\mathcal{R}_y + 10\frac{\mathcal{R}_y^2}{\mathcal{R}_x}}$$

$$L_{21} = \frac{N_1 N_2}{11\mathcal{R}_y + 10\frac{\mathcal{R}_y^2}{\mathcal{R}_x}}$$

By a similar method, it can be shown that $L_{12} = L_{21}$.

6. (a) $L_{m1} = L_{11} - L_{12} = 90 \text{ mH}$

$$L'_{12} = \left(\frac{N_1}{N_2}\right)^2 L_{12} = \left(\frac{100}{50}\right)^2 (2.5 \times 10^{-3}) = 10 \text{ mH}$$

$$r'_2 = \left(\frac{N_1}{N_2}\right)^2 r_2 = \left(\frac{100}{50}\right)^2 (2.5) = 10 \Omega$$

(b) $L_{m2} = L_{22} - L_{12} = 22.5 \text{ mH}$

$$L'_{11} = \left(\frac{N_2}{N_1}\right)^2 L_{11} = \left(\frac{50}{100}\right)^2 (10 \times 10^{-3}) = 2.5 \text{ mH}$$

$$r'_1 = \left(\frac{N_2}{N_1}\right)^2 r_1 = \left(\frac{50}{100}\right)^2 (10) = 2.5 \Omega$$

7. (a) $L_{12} = -\frac{N_1 N_2}{\mathcal{R}_m}$ (b) $\lambda_1 = L_{11} i_1 + L_{12} i_2$
 $\lambda_2 = L_{21} i_1 - L_{22} i_2$
(c) $\lambda_1 = L_{11} i_1 + L_{m1} (i_1 - i_2')$ (d) v_1 is unchanged
 $\lambda_2' = -L_{12}' i_2' + L_{m1} (i_1 - i_2')$ $v_2' = -r_2' i_2' + \frac{d\lambda_2'}{dt}$

8. $\tilde{V}_1 = \frac{10}{2\sqrt{2}} \angle 0^\circ = 3.54 \angle 0^\circ \text{ V}$
 $Z = r_1 + r_2' + j\omega_e (L_{11} + L_{12}') = 10 + 10 + j(2\pi)(30)(30 + 30) \times 10^{-3}$
 $= 20 + j 11.31 \Omega$

$$\tilde{I}_1 = \frac{\tilde{V}_1}{Z} = \frac{3.54 \angle 0^\circ}{20 + j 11.31} = 0.154 \angle -29.5^\circ \text{ A}$$

9. Since $\omega_e = 400$, $X_{m1} = 400 \Omega$. Neglecting the magnetizing current $i_1 = -i_2'$.

(a) $\tilde{V}_1 = \frac{2}{\sqrt{2}} \angle 0^\circ = \sqrt{2} \angle 0^\circ$

$$\tilde{I}_1 = \frac{\tilde{V}_1}{(r_1 + r_2 + R_L) + j\omega_e (L_{11} + L_{12})} = \frac{\sqrt{2} \angle 0^\circ}{4 + j(400)(0.02)} = 0.158 \angle -63.4^\circ \text{ A}$$

(b) $I_1 = \sqrt{2} 0.158 \cos(400t - 63.4^\circ)$

$$\begin{aligned}
 \mathbf{10.} \quad Z &= r_1 + \left(\frac{N_1}{N_2}\right)^2 (r_2 + R_L) + j \omega_e \left[L_{11} + \left(\frac{N_1}{N_2}\right)^2 L_{12} \right] \\
 &= 1 + \left(\frac{1}{2}\right)^2 (2 + 4) + j(400) \left[+ \left(\frac{1}{2}\right)^2 (0.04) \right] = 2.5 + j 8 \, \Omega
 \end{aligned}$$

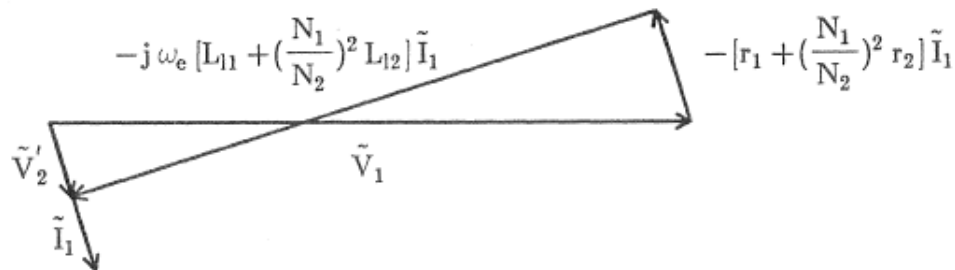
$$\tilde{I}_1 = \frac{\tilde{V}_1}{Z} = \frac{2 \angle 0^\circ}{2.5 + j 8} = 0.239 \angle -72.6^\circ \text{ A}$$

$$\tilde{I}_2' = -\tilde{I}_1 = -0.239 \angle -72.6^\circ \text{ A}$$

$$\tilde{V}_2' = -R_L' \tilde{I}_2' = -\left(\frac{1}{2}\right)^2 (4) (-0.239 \angle -72.6^\circ) = 0.239 \angle -72.6^\circ \text{ V}$$

Another method

$$\begin{aligned}
 \tilde{V}_2' &= \tilde{V}_1 - \tilde{I}_1 \left\{ r_1 + \left(\frac{N_1}{N_2}\right)^2 r_2 + j \omega_e \left[L_{11} + \left(\frac{N_1}{N_2}\right)^2 L_{12} \right] \right\} \\
 &= 2 \angle 0^\circ - 0.239 \angle -72.6^\circ (1.5 + j 8) \\
 &= 2 \angle 0^\circ - (1.5)(0.239 \angle -72.6^\circ) - j(8)(0.239 \angle -72.6^\circ) \\
 &= 2 \angle 0^\circ - 0.359 \angle -72.6^\circ - j 1.912 \angle -72.6^\circ = 0.239 \angle -72.6^\circ \text{ V}
 \end{aligned}$$



Phasor Diagram.

$$11. L_m(x) = \frac{k}{k_0 + x}$$

$$k = \frac{N^2 \mu_0 A_i}{2} = \frac{(500)^2 (4\pi \times 10^{-7})(4 \times 10^{-4})}{2} = 2\pi \times 10^{-5}$$

$$k_0 = \frac{l_i}{2\mu_{ri}} = \frac{20 \times 10^{-2}}{(2)(1000)} = 10^{-4}$$

$$L_m(x) = \frac{2\pi \times 10^{-5}}{10^{-4} + x} \text{ H}$$

The approximation for $x > 0$ is

$$L_m(x) = \frac{2\pi \times 10^{-5}}{x} \text{ H}$$

Now to find minimum value of x

$$\frac{2\pi \times 10^{-5}}{x} = 1.1 \frac{2\pi \times 10^{-5}}{10^{-4} + x}$$

Solving for x yields $x = 1$ mm. Thus, the approximate expression is 10% in error at $x = 1$ mm and less than this for $x > 1$ mm.

$$12. L_m(x) = \frac{k}{k_0 + x}$$

$$\frac{\partial L_m(x)}{\partial x} = \frac{-k}{(k_0 + x)^2}$$

$$v = r i + \left(L_1 + \frac{k}{k_0 + x}\right) \frac{di}{dt} - i \frac{k}{(k_0 + x)^2} \frac{dx}{dt}$$

$$v = r\sqrt{2} I_s \cos \omega_e t - \left(L_1 + \frac{k}{k_0 + t}\right) \omega_e \sqrt{2} I_s \sin \omega_e t - \sqrt{2} I_s \cos \omega_e t \left[\frac{k}{(k_0 + t)^2} \right]$$

Gathering terms

$$v = \left[r - \frac{k}{(k_0 + t)^2} \right] \sqrt{2} I_s \cos \omega_e t - \left(L_1 + \frac{k}{k_0 + t}\right) \omega_e \sqrt{2} I_s \sin \omega_e t$$

Taking the limit as $t \rightarrow \infty$

$$v = r \sqrt{2} I_s \cos \omega_e t - L_1 \omega_e \sqrt{2} I_s \sin \omega_e t$$

which is the voltage equation for a linear r-L circuit. In phasor form,

$$\tilde{V} = (r + j \omega_e L_1) \tilde{I}$$

$$13. \quad v = r i + \left[L_1 + L_m(\theta_r) \right] \frac{di}{dt} + i \frac{\partial L_m(\theta_r)}{\partial \theta_r} \frac{d\theta_r}{dt}$$

$$v = r i + \left[L_1 + L_A - L_B \cos 2\theta_r \right] \frac{di}{dt} + 2 \omega_r i L_B \sin 2\theta_r$$

$$14. \quad v_1 = r_1 i_1 + \frac{d\lambda_1}{dt}$$

$$v_2 = r_2 i_2 + \frac{d\lambda_2}{dt}$$

$$\lambda_1 = L_{11} i_1 + (L_{sr} \cos \theta_r) i_2$$

$$\lambda_2 = L_{22} i_2 + (L_{sr} \cos \theta_r) i_1$$

$$\frac{d\lambda_1}{dt} = \frac{\partial \lambda_1}{\partial i_1} \frac{di_1}{dt} + \frac{\partial \lambda_1}{\partial i_2} \frac{di_2}{dt} + \frac{\partial \lambda_1}{\partial \theta_r} \frac{d\theta_r}{dt}$$

$$= L_{11} \frac{di_1}{dt} + L_{sr} \cos \theta_r \frac{di_2}{dt} - i_2 \omega_r L_{sr} \sin \theta_r$$

$$\frac{d\lambda_2}{dt} = L_{22} \frac{di_2}{dt} + L_{sr} \cos \theta_r \frac{di_1}{dt} - i_1 \omega_r L_{sr} \sin \theta_r; \text{ thus,}$$

$$v_1 = r_1 i_1 + L_{11} \frac{di_1}{dt} + L_{sr} \cos \theta_r \frac{di_2}{dt} - i_2 \omega_r L_{sr} \sin \theta_r$$

$$v_2 = r_2 i_2 + L_{22} \frac{di_2}{dt} + L_{sr} \cos \theta_r \frac{di_1}{dt} - i_1 \omega_r L_{sr} \sin \theta_r$$