







1.3

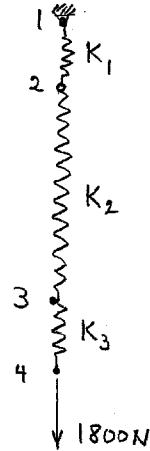
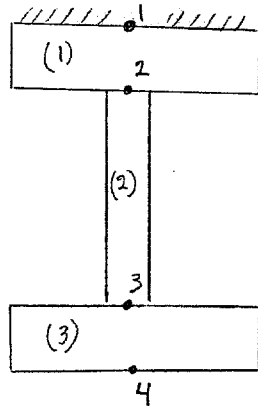
$$K = \frac{AE}{l}$$

$$K_1 = K_3 = \frac{(0.08)(0.006)(68.9 \times 10^9)}{0.025}$$

$$K_1 = K_3 = 1.32288 \times 10^9 \frac{N}{m}$$

$$K_2 = \frac{(0.02)(0.006)(68.9 \times 10^9)}{0.1}$$

$$K_2 = 0.08268 \times 10^9 \frac{N}{m}$$



$$10^9 \begin{bmatrix} 1.32288 & -1.32288 & 0 & 0 \\ -1.32288 & 1.32288 + 0.08268 & -0.08268 & 0 \\ 0 & -0.08268 & 0.08268 + 1.32288 & -1.32288 \\ 0 & 0 & -1.32288 & 1.32288 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 1800 \end{Bmatrix}$$

$$\begin{bmatrix} 1.40556 & -0.08268 & 0 \\ -0.08268 & 1.40556 & -1.32288 \\ 0 & -1.32288 & 1.32288 \end{bmatrix} \begin{Bmatrix} u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 1800 \times 10^{-9} \end{Bmatrix}$$

$$u_2 = 1.360668 \times 10^{-6} \text{ m}$$

$$u_3 = 2.313135 \times 10^{-5} \text{ m}$$

$$u_4 = 2.449202 \times 10^{-5} \text{ m}$$

$$\sigma^{(1)} = E \frac{u_2 - u_1}{l} = (68.9 \times 10^9) \left( \frac{1.360668 \times 10^{-6} - 0}{0.025} \right) = 3750000 = \underline{\underline{3.75 \text{ MPa}}}$$

as a check:  $\sigma^{(1)} = \frac{F}{A} = \frac{1800 \text{ N}}{(0.08)(0.006)} = \underline{\underline{3.75 \text{ MPa}}}$

$$\sigma^{(2)} = E \frac{u_3 - u_2}{l} = (68.9 \times 10^9) \left( \frac{2.313135 \times 10^{-5} - 1.360668 \times 10^{-6}}{0.1} \right) = \underline{\underline{15 \text{ MPa}}}$$

as a check  $\sigma^{(2)} = \frac{1800 \text{ N}}{(0.02)(0.006)} = \underline{\underline{15 \text{ MPa}}}$

$$\sigma^{(3)} = E \frac{u_4 - u_3}{l} = (68.9 \times 10^9) \left( \frac{2.449202 - 2.313135}{0.025} \right) \times 10^{-5} = \underline{\underline{3.75 \text{ MPa}}}$$

1.4

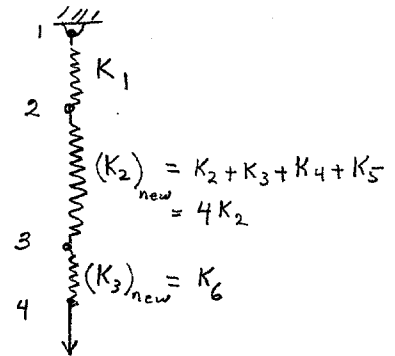
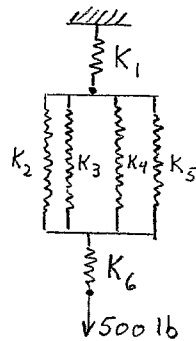
$$K_1 = K_6 = \frac{(4)(0.125)(28 \times 10^6)}{2}$$

$$K_1 = K_6 = 7 \times 10^6 \frac{\text{lb}}{\text{in}}$$

$$K_2 = K_3 = K_4 = K_5 = \frac{(0.625)(0.125)(28 \times 10^6)}{8}$$

$$K_2 = 273438 \frac{\text{lb}}{\text{in}}$$

$$(K_2)_{\text{new}} = (4)(273438) = 1093750 \frac{\text{lb}}{\text{in}}$$



$$\begin{bmatrix} 7 \times 10^6 & 0 & 0 & 0 \\ 0 & -7 \times 10^6 & 0 & 0 \\ -7 \times 10^6 & 7 \times 10^6 + 1093750 & 0 & 0 \\ 0 & 0 & -1093750 & 1093750 + 7 \times 10^6 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 500 \end{Bmatrix}$$

$$\begin{bmatrix} 8093750 & -1093750 & 0 & 0 \\ -1093750 & 8093750 & -7 \times 10^6 & 0 \\ 0 & -7 \times 10^6 & 7 \times 10^6 & 0 \\ 0 & 0 & 0 & 7 \times 10^6 \end{bmatrix} \begin{Bmatrix} u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 500 \end{Bmatrix}$$

$$u_2 = 7.142857 \times 10^{-5} \text{ in}$$

$$u_3 = 5.285714 \times 10^{-4} \text{ in}$$

$$u_4 = 6 \times 10^{-4} \text{ in}$$



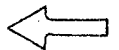
$$\sigma^{(1)} = E \left( \frac{u_2 - u_1}{l} \right) = 28 \times 10^6 \left( \frac{7.142857 \times 10^{-5} \text{ in}}{2} \right) = 1000 \frac{\text{lb}}{\text{in}^2}$$

as a check:  $\sigma^{(1)} = \frac{F}{A} = \frac{500}{(4)(0.125)} = 1000 \frac{\text{lb}}{\text{in}^2}$

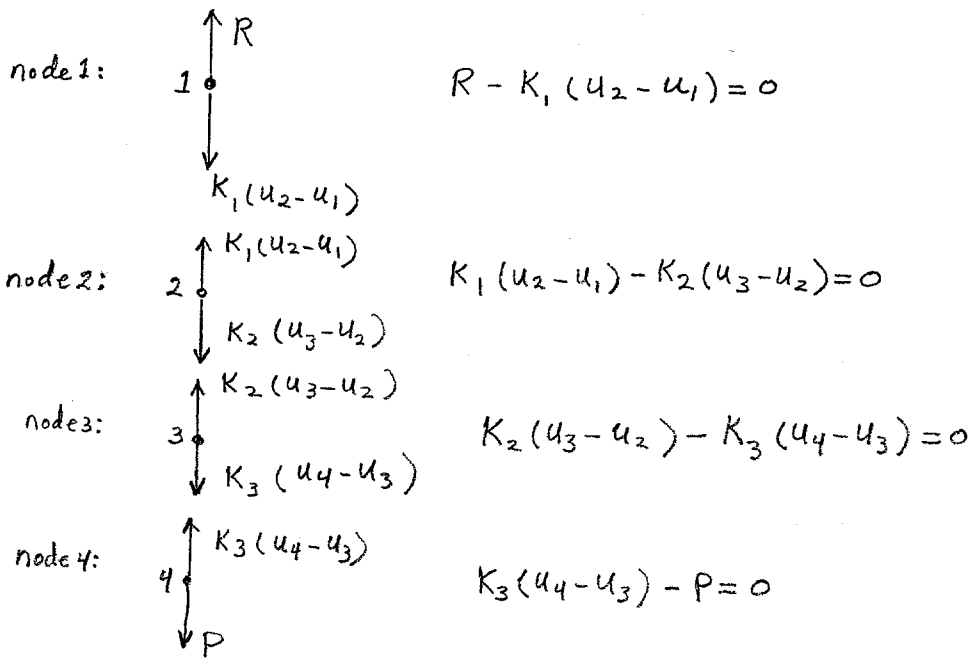
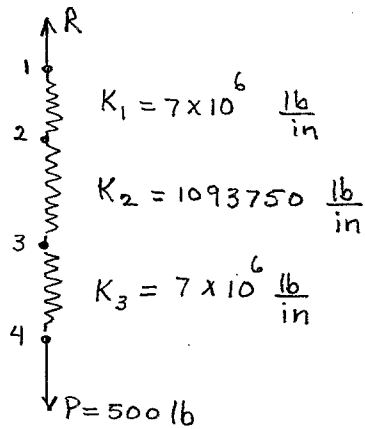
$$\sigma^{(2)} = E \left( \frac{u_3 - u_2}{l} \right) = 28 \times 10^6 \left( \frac{5.285714 \times 10^{-4} - 7.142857 \times 10^{-5}}{8} \right) = 1600 \frac{\text{lb}}{\text{in}^2}$$

as a check:  $\sigma^{(2)} = \frac{500}{(2.5)(0.125)} = 1600 \frac{\text{lb}}{\text{in}^2}$

$$\sigma^{(3)} = E \left( \frac{u_4 - u_3}{l} \right) = 28 \times 10^6 \left( \frac{6 \times 10^{-4} - 5.285714 \times 10^{-4}}{2} \right) = 1000 \frac{\text{lb}}{\text{in}^2}$$



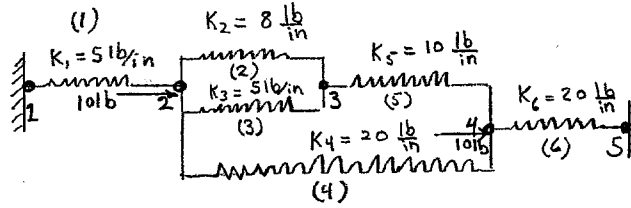
1.5



In matrix form:

$$\begin{bmatrix}
 K_1 & -K_1 & & & \\
 -K_1 & K_1 + K_2 & -K_2 & & \\
 & -K_2 & K_2 + K_3 & & \\
 & & & K_3 & \\
 & & & & -K_3 & K_3
 \end{bmatrix}
 \begin{Bmatrix}
 u_1 \\
 u_2 \\
 u_3 \\
 u_4
 \end{Bmatrix}
 =
 \begin{Bmatrix}
 -R \\
 0 \\
 0 \\
 P
 \end{Bmatrix}$$

1.6



Size of the global matrix: 5x5

$$[K]^{(1)} = \begin{bmatrix} 5 & -5 \\ -5 & 5 \end{bmatrix} \begin{matrix} \text{①} & \text{②} \\ \text{②} & \text{①} \end{matrix}$$

$$[K]^{(2)} = \begin{bmatrix} 8 & -8 \\ -8 & 8 \end{bmatrix} \begin{matrix} \text{②} & \text{③} \\ \text{③} & \text{②} \end{matrix}$$

$$[K]^{(3)} = \begin{bmatrix} 5 & -5 \\ -5 & 5 \end{bmatrix} \begin{matrix} \text{②} & \text{③} \\ \text{③} & \text{②} \end{matrix}$$

$$[K]^{(4)} = \begin{bmatrix} 20 & -20 \\ -20 & 20 \end{bmatrix} \begin{matrix} \text{②} & \text{④} \\ \text{④} & \text{②} \end{matrix}$$

$$[K]^{(5)} = \begin{bmatrix} 10 & -10 \\ -10 & 10 \end{bmatrix} \begin{matrix} \text{③} & \text{④} \\ \text{④} & \text{③} \end{matrix}$$

$$[K]^{(6)} = \begin{bmatrix} 20 & -20 \\ -20 & 20 \end{bmatrix} \begin{matrix} \text{④} & \text{⑤} \\ \text{⑤} & \text{④} \end{matrix}$$

$$[K]^{(6)} = \begin{bmatrix} 5 & -5 & & & \\ -5 & 5+8+5+20 & -8-5 & -20 & \\ & -8-5 & 8+5+10 & -10 & \\ & -20 & -10 & 20+10+20 & -20 \\ & & & -20 & 20 \end{bmatrix}$$

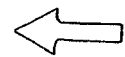
applying B.Cs and loads;  $u_1 = u_5 = 0$   $F_2 = 10 \text{ lb}$   $F_4 = 10 \text{ lb}$

$$\begin{bmatrix} 38 & -13 & -20 \\ -13 & 23 & -10 \\ -20 & -10 & 50 \end{bmatrix} \begin{Bmatrix} u_2 \\ u_3 \\ u_4 \end{Bmatrix} = \begin{Bmatrix} 10 \\ 0 \\ 10 \end{Bmatrix}$$

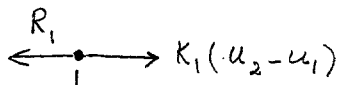
$u_2 = 0.962 \text{ in}$

$u_3 = 0.874 \text{ in}$

$u_4 = 0.760 \text{ in}$

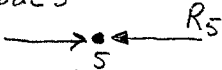


node 1:

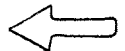


$R_1 = 5(0.962 - 0) = 4.8 \text{ lb}$

node 5



$R_5 = 20(0.760 - 0) = 15.2 \text{ lb}$



$K(u_4 - u_5)$

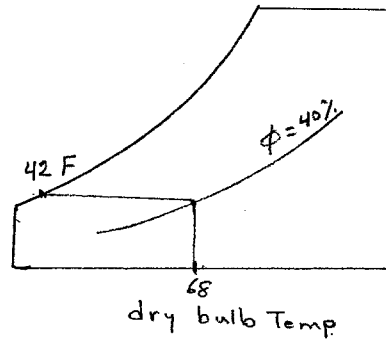
note also as a check,  $R_1 + R_5 = \sum F_{\text{external}} \quad 4.8 + 15.2 = 10 + 10$





1.9

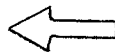
with the help of a psychometric chart, using a dry bulb Temp of 68°F and  $\phi = 40\%$ , we identify condensation temperature to be 42°F. Thus condensation will occur between surfaces 4 and 5.



1.10

$$1000 \begin{bmatrix} \frac{1}{1000} & 0 \\ \frac{1.47}{1000} & -1.47 \\ -1.47 & 1.47 + 0.053 \\ -0.053 & 0.053 + 2.22 \\ -2.22 & 2.22 + 1.47 \\ -1.47 & 1.47 \\ 0 & \frac{1}{1000} \end{bmatrix} \begin{Bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{Bmatrix} = \begin{Bmatrix} 15 \\ 0 \\ 0 \\ 0 \\ 70 \end{Bmatrix}$$

$$\{T\} = \begin{Bmatrix} 15 \\ 16.81 \\ 68.99 \\ 70 \end{Bmatrix} \text{ } ^\circ\text{F}$$



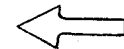
$$\dot{q} = UA \Delta T$$

as an example:

$$\dot{q} = (1.47)(1000)(70 - 68.99) = 2660 \frac{\text{Btu}}{\text{hr}}$$

or

$$\dot{q} = (1.47)(1000)(16.81 - 15) = 2660 \frac{\text{Btu}}{\text{hr}}$$



1.11

$$22.5 \begin{bmatrix} \frac{1}{22.5} & 0 \\ 5.88 & -5.88 \\ -5.88 & 5.88 + 2.56 \\ & -2.56 \\ & & 2.56 + 1.47 \\ & & & -1.47 \\ & & & & \frac{1}{22.5} \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \begin{bmatrix} 20 \\ 0 \\ 0 \\ 70 \end{bmatrix}$$

$$\{T\} = \begin{Bmatrix} 20 \\ 26.85 \\ 42.59 \\ 70 \end{Bmatrix} \text{ } ^\circ\text{F}$$

$$q = U_1 A \Delta T = (5.88)(22.5)(26.85 - 20) = 910 \frac{\text{Btu}}{\text{hr}}$$

or as another example:

$$q = U_2 A \Delta T = (2.56)(22.5)(42.59 - 26.85) = 910 \frac{\text{Btu}}{\text{hr}}$$

or

$$q = \frac{1}{\sum \text{Resistance}} A (T_{in} - T_{out}) = \frac{1}{(0.17 + 0.39 + 0.68)} (22.5)(70 - 20)$$

$$q = 910 \frac{\text{Btu}}{\text{hr}}$$

1.12

$$(A_1)_c = (A_5)_c = \left(\frac{12+10.5}{2}\right)(3) - 3 \frac{\pi}{4} (0.5)^2 = 33.161 \text{ in}^2$$

$$(A_2)_c = (A_4)_c = \frac{(10.5+9)}{2}(3) - 3 \frac{\pi}{4} (0.5)^2 = 28.661 \text{ in}^2$$

$$(A_3)_c = (9)(3) - 3 \frac{\pi}{4} (0.5)^2 = 26.411 \text{ in}^2$$

$$(K_1)_c = (K_5)_c = \frac{(33.161)(3.27 \times 10^6)}{6} = 18,072,745 \frac{\text{lb}}{\text{in}}$$

$$(K_2)_c = (K_4)_c = \frac{(28.661)(3.27 \times 10^6)}{6} = 15,620,245 \frac{\text{lb}}{\text{in}}$$

$$(K_3)_c = \frac{(26.411)(3.27 \times 10^6)}{4} = 21,590,992 \frac{\text{lb}}{\text{in}}$$

$$(K_1)_s = (K_2)_s = (K_4)_s = (K_5)_s = \frac{(3)\left(\frac{\pi}{4}\right)(0.5)^2(29 \times 10^6)}{6} = 2,847,068 \frac{\text{lb}}{\text{in}}$$

$$(K_3)_s = \frac{(3)\left(\frac{\pi}{4}\right)(0.5)^2(29 \times 10^6)}{4} = 4,270,602 \frac{\text{lb}}{\text{in}}$$

The Combined stiffnesses:

$$K_1 = K_5 = 18,072,745 + 2,847,068 = 20,919,813$$

$$K_2 = K_4 = 15,620,245 + 2,847,068 = 18,467,313$$

$$K_3 = 21,590,992 + 4,270,602 = 25,861,594$$

$\frac{1}{20,919,813}$	$\frac{0}{-20,919,813}$						
$\frac{0}{-20,919,813}$	$\frac{0}{20,919,813}$	$\frac{0}{+18,467,313}$	$\frac{0}{-18,467,313}$				
		$\frac{0}{-18,467,313}$	$\frac{0}{18,467,313}$	$\frac{0}{+25,861,594}$	$\frac{0}{-25,861,594}$		
				$\frac{0}{-25,861,594}$	$\frac{0}{25,861,594}$	$\frac{0}{+18,467,313}$	$\frac{0}{-18,467,313}$
						$\frac{0}{-18,467,313}$	$\frac{0}{18,467,313}$
							$\frac{0}{20,919,813}$
							$\frac{0}{-20,919,813}$

$$\begin{Bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -1000 \end{Bmatrix}$$

$$u_1 = 0$$

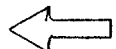
$$u_2 = -4.78016 \times 10^{-5} \text{ in}$$

$$u_3 = -1.01951 \times 10^{-4} \text{ in}$$

$$u_4 = -1.40618 \times 10^{-4}$$

$$u_5 = -1.94768 \times 10^{-4} \text{ in}$$

$$u_6 = -2.42570 \times 10^{-4} \text{ in}$$



1.12  
Cont.

$$\sigma_{\text{concrete}}^{(1)} = E_c \frac{(u_2 - u_1)}{l} = \frac{(3.27 \times 10^6)(-4.78016 \times 10^{-5})}{6} = \underline{\underline{26 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

$$\sigma_{\text{steel}}^{(1)} = E_s \frac{(u_2 - u_1)}{l} = \underline{\underline{231 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

as a check:

$$\sigma_{\text{concrete}}^{(1)} (A_1)_c + \sigma_s^{(1)} (A_1)_s = (26)(33.161) + (231)(3)\left(\frac{\pi}{4}\right)(0.5)^2 = \underline{\underline{1000 \text{ lb}}}$$

$$\sigma_c^{(2)} = E_c \frac{(u_3 - u_2)}{l} = \frac{(3.27 \times 10^6)(-1.01951 \times 10^{-4} + 4.78016 \times 10^{-5})}{6} = \underline{\underline{30 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

$$\sigma_s^{(2)} = 231 \frac{\text{lb}}{\text{in}^2} \text{ C}$$

check:  $\sigma_c^{(2)} (A_2)_c + \sigma_s^{(2)} (A_2)_s = (30)(28.661) + (231)(3)\left(\frac{\pi}{4}\right)(0.5)^2 = 1000 \text{ lb}$

$$\sigma_c^{(3)} = E_c \frac{(u_4 - u_3)}{l} = \frac{(3.27 \times 10^6)(-1.40618 \times 10^{-4} + 1.01951 \times 10^{-4})}{4} = \underline{\underline{32 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

$$\sigma_s^{(3)} = E_s \frac{(u_4 - u_3)}{l} = \frac{(29 \times 10^6)(-1.40618 \times 10^{-4} + 1.01951 \times 10^{-4})}{4} = \underline{\underline{280 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

check:  $\sigma_c^{(3)} (A_3)_c + \sigma_s^{(3)} (A_3)_s = (32)(26.411) + (280)(3)\left(\frac{\pi}{4}\right)(0.5)^2 = 1000 \text{ lb}$

$$\sigma_c^{(4)} = E_c \frac{(u_5 - u_4)}{l} = \frac{(3.27 \times 10^6)(-1.94768 \times 10^{-4} + 1.40618 \times 10^{-4})}{6} = \underline{\underline{30 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

$$\sigma_s^{(4)} = 231 \frac{\text{lb}}{\text{in}^2} \text{ C}$$

$$\sigma_c^{(5)} = E_c \frac{(u_6 - u_5)}{l} = \frac{(3.27 \times 10^6)(-2.42570 \times 10^{-4} + 1.94768 \times 10^{-4})}{6} = \underline{\underline{26 \frac{\text{lb}}{\text{in}^2} \text{ C}}}$$

$$\sigma_s^{(5)} = 231 \frac{\text{lb}}{\text{in}^2} \text{ C}$$

note  $\sigma_c^{(1)} = \sigma_c^{(5)}$  and  $\sigma_s^{(2)} = \sigma_s^{(4)}$  as expected.

$$\Lambda^{(e)} = \frac{A_{\text{avg}} E}{2l} (u_{i+1} - u_i)^2$$

$$\Lambda_{\text{total}} = \Lambda^{(1)} + \Lambda^{(2)} + \Lambda^{(3)} + \Lambda^{(4)} + \Lambda^{(5)}$$

$$\Lambda^{(1)} = \Lambda^{(5)} = \frac{(A_1)_c E_c}{2l} (u_{i+1} - u_i)^2 + \frac{(A_1)_s E_s}{2l} (u_{i+1} - u_i)^2$$

$$= \frac{(A_1)_c E_c + (A_1)_s E_s}{2l} (u_2 - u_1)^2$$

$$\Lambda^{(1)} = \left[ \frac{(33.161)(3.27 \times 10^6) + 3 \left(\frac{\pi}{4}\right) (0.5)^2 (29 \times 10^6)}{(2)(6)} \right] \left[ -4.78016 \times 10^{-5} \right]^2 = 0.024 \text{ lb.in}$$

$$\Lambda^{(5)} = \left[ \frac{(33.161)(3.27 \times 10^6) + 3 \left(\frac{\pi}{4}\right) (0.5)^2 (29 \times 10^6)}{(2)(6)} \right] \left[ (-2.4257 + 1.94768) \times 10^{-4} \right]^2 = 0.024 \checkmark$$

$$\Lambda^{(2)} = \frac{(A_2)_c E_c + (A_2)_s E_s}{2l} (u_3 - u_2)^2$$

$$= \left[ \frac{(28.661)(3.27 \times 10^6) + 3 \left(\frac{\pi}{4}\right) (0.5)^2 (29 \times 10^6)}{2(6)} \right] \left[ (-1.01951 \times 10^{-4} + 4.78016 \times 10^{-5}) \right]^2 = 0.027$$

$$\Lambda^{(4)} = \left[ \frac{(28.661)(3.27 \times 10^6) + 3 \left(\frac{\pi}{4}\right) (0.5)^2 (29 \times 10^6)}{2(6)} \right] \left[ (-1.94768 + 1.40618) \times 10^{-4} \right]^2 = 0.027 \checkmark$$

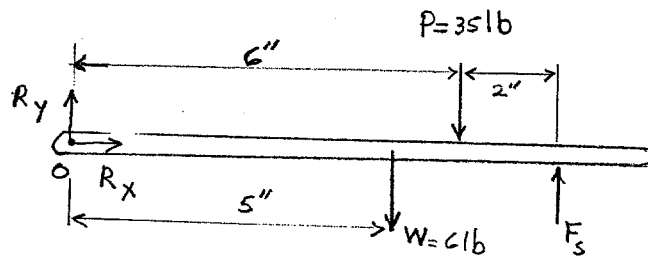
$$\Lambda^{(3)} = \frac{(A_3)_c E_c + (A_3)_s E_s}{2l} (u_4 - u_3)^2$$

$$\Lambda^{(3)} = \left[ \frac{(26.411)(3.27 \times 10^6) + 3 \left(\frac{\pi}{4}\right) (0.5)^2 (29 \times 10^6)}{2(4)} \right] \left[ (-1.40618 + 1.01951) \times 10^{-4} \right]^2$$

$$= 0.019 \text{ lb.in}$$

$$\Lambda_{\text{total}} = (2)(0.024) + 0.019 + 2(0.027) = \underline{\underline{0.121 \text{ lb.in}}} \leftarrow$$

1.14



(a)  $\oplus \uparrow \sum M_o = 0$

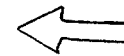
$$(-6 \text{ lb})(5 \text{ in}) + (35 \text{ lb})(6 \text{ in}) + F_s (8 \text{ in}) = 0$$

$$F_s = 30 \text{ lb}$$

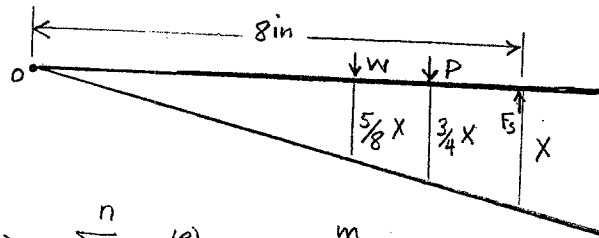
$$F_s = KX$$

$$30 \text{ lb} = 60 X$$

$$X = 0.5 \text{ in}$$



(b)



$$\frac{\partial \pi}{\partial u_i} = \frac{\partial}{\partial u_i} \sum_{i=1}^n \Lambda^{(e)} - \frac{\partial}{\partial u_i} \sum_{i=1}^m F_i u_i = 0$$

$$\frac{\partial}{\partial X} \left( \frac{1}{2} K X^2 \right) - \frac{\partial}{\partial X} \left( 35 \left( \frac{3}{4} X \right) \right) - (6) \left( \frac{5}{8} X \right) = 0$$

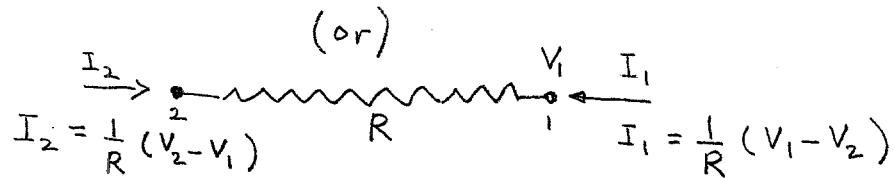
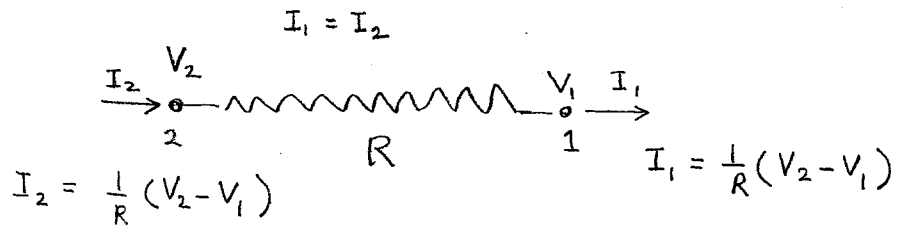
$$KX - (35) \left( \frac{3}{4} \right) - (6) \left( \frac{5}{8} \right) = 0$$

$$X = \frac{(35) \left( \frac{3}{4} \right) + (6) \left( \frac{5}{8} \right)}{60}$$

$$X = 0.5 \text{ in}$$



1.15



Because of the fact that charge is conserved in a circuit (Kirchhoff's current law), at any time, the algebraic sum of the currents entering any node must be zero. Thus we can write

$$I_1 = \frac{1}{R} (V_1 - V_2)$$

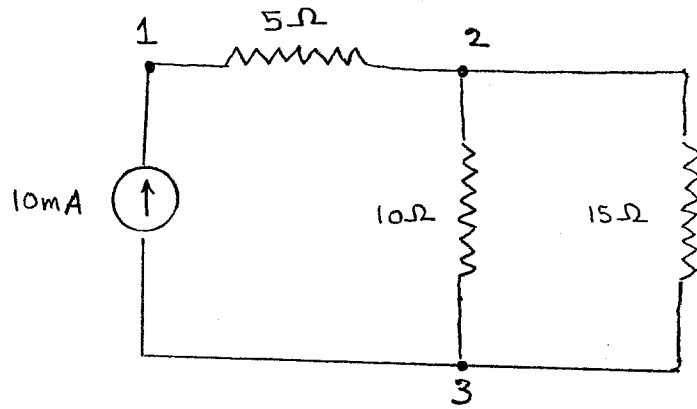
$$I_2 = \frac{1}{R} (V_2 - V_1)$$

Note  $I_1 + I_2 = 0$

In matrix form:

$$\frac{1}{R} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} V_1 \\ V_2 \end{Bmatrix} = \begin{Bmatrix} I_1 \\ I_2 \end{Bmatrix}$$

1.16



$$[K]^{(1)} = \frac{1}{5} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

$$[K]^{(2)} = \frac{1}{10} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

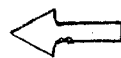
$$[K]^{(3)} = \frac{1}{15} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}; \text{ Apply } V_3 = 0 \text{ as a boundary condition}$$

$$\begin{bmatrix} \frac{1}{5} & -\frac{1}{5} & 0 \\ -\frac{1}{5} & \frac{1}{5} + \frac{1}{10} + \frac{1}{15} & -\frac{1}{10} - \frac{1}{15} \\ 0 & -\frac{1}{10} - \frac{1}{15} & \frac{1}{10} + \frac{1}{15} \end{bmatrix} \begin{Bmatrix} V_1 \\ V_2 \\ V_3 \end{Bmatrix} = \begin{Bmatrix} 0.01 \\ 0 \\ 0 \end{Bmatrix}$$

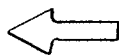
$$V_1 = 0.11$$

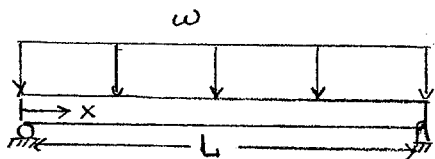
$$V_2 = 0.06$$

$$\underline{\underline{V_1 - V_2 = 0.05 \text{ Volts}}}$$



$$\underline{\underline{V_2 - V_3 = 0.06 \text{ Volts}}}$$





$$\frac{d^2 Y}{dx^2} = \frac{M(x)}{EI} = \frac{wx(L-x)}{2EI}$$

$$\frac{dY}{dx} = \frac{1}{2EI} \left( \frac{wX^2 L}{2} - \frac{wX^3}{3} \right) + C_1$$

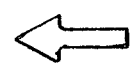
$$Y = \frac{1}{2EI} \left( \frac{wX^3 L}{6} - \frac{wX^4}{12} \right) + C_1 X + C_2$$

Applying Boundary Conditions:

$$Y=0 \quad \text{at} \quad x=0 \quad C_2=0$$

$$Y=0 \quad \text{at} \quad x=L \quad C_1 = -\frac{wL^3}{24EI}$$

$$Y_{\text{exact}} = \frac{-wX}{24EI} (X^3 - 2LX^2 + L^3)$$



(a) Note that the assumed Solution satisfies the boundary Conditions.  $Y = C_1 \left[ \left(\frac{x}{L}\right)^2 - \left(\frac{x}{L}\right) \right]$

$$\frac{dY}{dx} = C_1 \left[ \frac{2x}{L^2} - \frac{1}{L} \right]$$

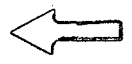
$$\frac{d^2 Y}{dx^2} = C_1 \left( \frac{2}{L^2} \right)$$

$$\frac{2C_1}{L^2} - \frac{wx(L-x)}{2EI} = R$$

We may force the error function to equal zero at  $x = \frac{L}{2}$

$$\frac{2C_1}{L^2} - \frac{w \frac{L}{2} (L - \frac{L}{2})}{2EI} = 0 \quad \rightarrow \quad C_1 = \frac{wL^4}{16EI}$$

$$Y = \frac{wL^4}{16EI} \left[ \left(\frac{x}{L}\right)^2 - \left(\frac{x}{L}\right) \right]$$



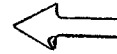
1.17  
Cont.

$$(b) \int_0^L R dx = 0$$

$$\int_0^L \left[ \frac{2C_1}{L^2} - \frac{w x (L-x)}{2EI} \right] dx = 0$$

$$\frac{2C_1}{L^2} L - \frac{w}{2EI} \left( \frac{L^3}{2} - \frac{L^3}{3} \right) = 0 \rightarrow C_1 = \frac{wL^4}{24EI}$$

$$Y = \frac{wL^4}{24EI} \left( \left( \frac{x}{L} \right)^2 - \left( \frac{x}{L} \right) \right)$$



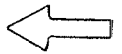
For W24x104 Beam  $I = 3100 \text{ in}^4$ ;  $E = 29 \times 10^6 \frac{\text{lb}}{\text{in}^2}$

Exact

$$Y_{\max} = \frac{-5wL^4}{384EI} = \frac{-5 \left( 5000 \frac{\text{lb}}{\text{ft}} \times \frac{1 \text{ ft}}{12 \text{ in}} \right) \left( 20 \text{ ft} \times \frac{12 \text{ in}}{\text{ft}} \right)^4}{(384) \left( 29 \times 10^6 \frac{\text{lb}}{\text{in}^2} \right) (3100 \text{ in}^4)} = \underline{\underline{-0.20 \text{ in}}}$$

Collocation

$$Y_{\max} = \frac{-wL^4}{64EI} = \frac{- \left( 5000 \frac{\text{lb}}{\text{ft}} \times \frac{1 \text{ ft}}{12 \text{ in}} \right) \left( 20 \text{ ft} \times \frac{12 \text{ in}}{\text{ft}} \right)^4}{(64) \left( 29 \times 10^6 \frac{\text{lb}}{\text{in}^2} \right) (3100 \text{ in}^4)} = \underline{\underline{-0.24 \text{ in}}}$$



Subdomain

$$Y_{\max} = \frac{-wL^4}{96EI} = \frac{- \left( 5000 \frac{\text{lb}}{\text{ft}} \times \frac{1 \text{ ft}}{12 \text{ in}} \right) \left( 20 \text{ ft} \times \frac{12 \text{ in}}{\text{ft}} \right)^4}{(96) \left( 29 \times 10^6 \frac{\text{lb}}{\text{in}^2} \right) (3100 \text{ in}^4)} = \underline{\underline{-0.16 \text{ in}}}$$

1.18

See Section 1.7

1.19

$$\mu \frac{d^2 u}{dy^2} = \frac{dP}{dx}$$

$$\frac{du}{dy} = \frac{1}{\mu} \frac{dP}{dx} y + C_1$$

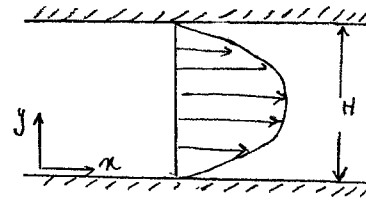
$$u(y) = \frac{1}{\mu} \frac{dP}{dx} \frac{y^2}{2} + C_1 y + C_2$$

applying B.C.s  $u(0) = 0$  and  $u(H) = 0$

$$0 = 0 + 0 + C_2 \quad \text{and} \quad 0 = \frac{1}{\mu} \frac{dP}{dx} \frac{H^2}{2} + C_1 H$$

$$C_2 = 0 \quad \text{and} \quad C_1 = -\frac{H}{2\mu} \frac{dP}{dx}$$

$$\underline{\underline{u(y) = -\frac{1}{2\mu} \frac{dP}{dx} (Hy - y^2)}}$$



note <sup>because</sup> Pressure drops in the direction of flow,  $\frac{dP}{dx} < 0$  in velocity equation.

$$(a) \quad \mu \frac{d^2 u}{dy^2} = \frac{dP}{dx}$$

$$u_{\text{assumed}} = C_1 \sin\left(\frac{\pi y}{H}\right)$$

note the assumed solution satisfies the boundary conditions.

$$\frac{du}{dy} = \frac{d}{dy} \left( C_1 \sin\left(\frac{\pi y}{H}\right) \right) = C_1 \frac{\pi}{H} \cos\left(\frac{\pi y}{H}\right)$$

$$\frac{d^2 u}{dy^2} = \frac{d}{dy} \left( C_1 \frac{\pi}{H} \cos\left(\frac{\pi y}{H}\right) \right) = -C_1 \left(\frac{\pi}{H}\right)^2 \sin\left(\frac{\pi y}{H}\right)$$

$$\mu \left[ -C_1 \left(\frac{\pi}{H}\right)^2 \sin\left(\frac{\pi y}{H}\right) \right] - \frac{dP}{dx} = R$$

We may force the error function to equal zero at  $y = \frac{H}{2}$

$$\mu \left[ -C_1 \left(\frac{\pi}{H}\right)^2 \sin\left(\frac{\pi}{2}\right) \right] - \frac{dP}{dx} = 0$$

$$C_1 = -\frac{H^2}{\mu \pi^2} \frac{dP}{dx}$$

$$\text{then, } \underline{\underline{u(y) = -\frac{H^2}{\mu \pi^2} \frac{dP}{dx} \left( \sin\left(\frac{\pi y}{H}\right) \right)}}$$

